

Original Research

Hexagonal Microstrip MIMO Antenna with Defected Ground Structures for ISM/IoT Application

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Article History

Received:
6 November 2024

Revised:
18 February 2025

Accepted:
15 May 2025

Published in Issue:
30 June 2026

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Abstract:

In this manuscript, an original multiple-input multiple-output (MIMO) array antenna is proposed. The proposed array consists of two mirror-image elements placed adjacently. The proposed MIMO antenna is designed on the Rogers 4003C substrate with dimensions of $54 \times 26 \times 0.508 \text{ mm}^3$. The recommended MIMO antenna exhibits a fractional impedance bandwidth of 13.79% (5.4 – 6.2 GHz), and achieves an element isolation greater than 22 dB. The proposed MIMO array demonstrates a gain of 5 dB with an efficiency of 95% at 5.8 GHz. Additionally, the MIMO array has a channel capacity loss less than 0.2 b/s/Hz, an envelope correlation coefficient of ≤ 0.02 , a diversity gains of $\geq 9.96 \text{ dB}$, and a mean effective gain ratio between elements of 1 dB. Due to its optimal operating frequency, high efficiency, and compact size, this antenna is an appropriate candidate for ISM/IoT applications.

Keywords: Decoupling network; Defected ground structure; ISM/IoT applications; Microstrip MIMO antenna; Mutual coupling

Cite this article: Talebi F, Rezaei P, Kiani S. Hexagonal Microstrip MIMO Antenna with Defected Ground Structures for ISM/IoT Application. *Majlesi J. Electr. Eng.* 2026;20(2): 136-149. <https://doi.org/10.57647/mjee.2026.2002.10>

1. Introduction

In recent years, wireless communications have witnessed significant revolutionary advancements. The field of wireless communication systems encompasses a wide range of topics, including the development of communication chains, waveform design, interference and traffic management, channel modeling, compensating for radio hardware imperfections, symbol and bit recovery, and the enhancement of wireless security [1, 2, 3]. In the era of digital communication, the widespread use of platforms among new generations necessitates those wireless systems provide the highest data transmission rates, robust connectivity, enhanced reliability, and strong security measures [4, 5]. In recent years, MIMO antennas have obtained significant attention in non-line-of-sight wireless communications because they can utilize multiple paths for transmitting and receiving signals [6, 7]. MIMO antennas are commonly used to enhance reliability and increase data rates, thereby reducing interference from other wireless devices [8]. MIMO antennas are suitable

for communication systems like LTE and Wi-Fi [9].

One challenge of MIMO antennas is the need to decrease mutual coupling between elements. When designing MIMO antennas, this parameter must be significantly reduced to ensure each antenna operates independently and efficiently [10, 11]. Some methods for controlling mutual coupling include decoupling networks, split-ring resonators (SRRs), complementary split-ring resonators (CSRRs), varactor diodes, and electromagnetic bandgap structures [12, 13].

Varactor diodes are integrated tuning components that help control frequency and radiation patterns. They utilize a dielectric material, which enhances isolation. However, incorporating varactor diodes can increase complexity, reduce overall efficiency, and require high voltage toggling between the ON and OFF states [14]. Split Ring Resonators (SRRs) enhance antenna performance by creating a resonant effect for precise frequency calibration. Complementary Split-Ring Resonators (CSRRs) are essentially the inverse of SRRs; they provide high

isolation between closely spaced antennas, reduce mutual coupling, and improve the efficiency of Multiple Input Multiple Output (MIMO) systems. However, the resonant frequency of these components is sensitive to external conditions, and there can be challenges in their design and fabrication [15, 16].

Another method for reducing mutual coupling is the use of defected ground structures (DGS). DGSs have been applied in various communication devices, such as antennas [17, 18], planar waveguides [19], sensors [20, 21, 22], filters [23, 24], oscillators [25], and biosensors [26, 27, 28], to enhance performance. In recent years, antenna designers have been focused on developing wideband and wearable antennas, particularly for MIMO antenna [29, 30, 31]. Consequently, substantial research has been conducted in the areas of reconfigurable and wearable MIMO antennas [32], as well as UWB MIMO [33], positioning them as promising options for next-generation antennas [34, 35].

In this paper, an innovative MIMO microstrip array antenna is presented. The proposed antenna consists of two incomplete hexagonal patches, both of which are fed by a $50\ \Omega$ microstrip line. The antenna is placed on the Rogers 4003C board, with a thickness of 0.508 mm, a relative permittivity of 3.38, and a loss tangent of 0.0027. The primary challenge in MIMO antennas is achieving sufficient isolation between the antenna elements. This paper discusses a solution where the antenna elements are positioned on a defected ground structure (DGS) to minimize mutual coupling while maintaining a compact dimension [36]. Consequently, the proposed MIMO antenna operates within the frequency range of 5.4 – 6.2 GHz. It offers high isolation, a compact design, and low cost, making it well-suited for Internet of Things and Industrial, Scientific, and Medical (ISM/IOT) applications.

Section 2 discusses the planning steps for a single microstrip antenna, including an analysis of the S_{11} parameters at each stage, with surface current measure-

ments taken at 5.8 GHz. Section 3 presents the designed sample and the constructed prototype of the proposed MIMO antenna, illustrated with S-parameters and radiation patterns. Finally, section 4 details the obtained results.

2. Designing steps of single microstrip element

The modified microstrip antenna is illustrated in figure 1. The Rogers 4003C substrate is utilized due to its low cost, robustness, and availability. The initial step in designing a single microstrip antenna is to determine the patch parameters using equations (1)-(5) [37]. This research utilizes the DGS to improve isolation by altering the return path of surface current at the operating frequency, based on previous studies conducted by [38, 39, 40], and [41]. The second step involves optimizing the antenna gain by loading slot on the patch, allowing the surface current to meander while maintaining the dimensions. In the third step, a slot is added to the patch, redirecting the surface current along the patch. Consequently, this increases the bandwidth and shifts the resonance frequency closer to 5.8 GHz, optimizing the antenna for ISM/IoT applications. The final goal of this article is to design a MIMO antenna. Therefore, the ground structure is modified to enhance isolation, gain, and efficiency. Figure 2 presents the design evolution of the single-element microstrip antenna, which features a defective ground structure. It includes an analysis of the S-parameter diagram and the variations in resonant frequencies. Additionally, the simulated far-field radiation pattern and gain of the single-element antenna is 3.42 dB at 5.8 GHz. Furthermore, figure 3 illustrates the surface current distributions for the single-element antenna for both the (top/bottom layer) at a frequency of 5.8 GHz.

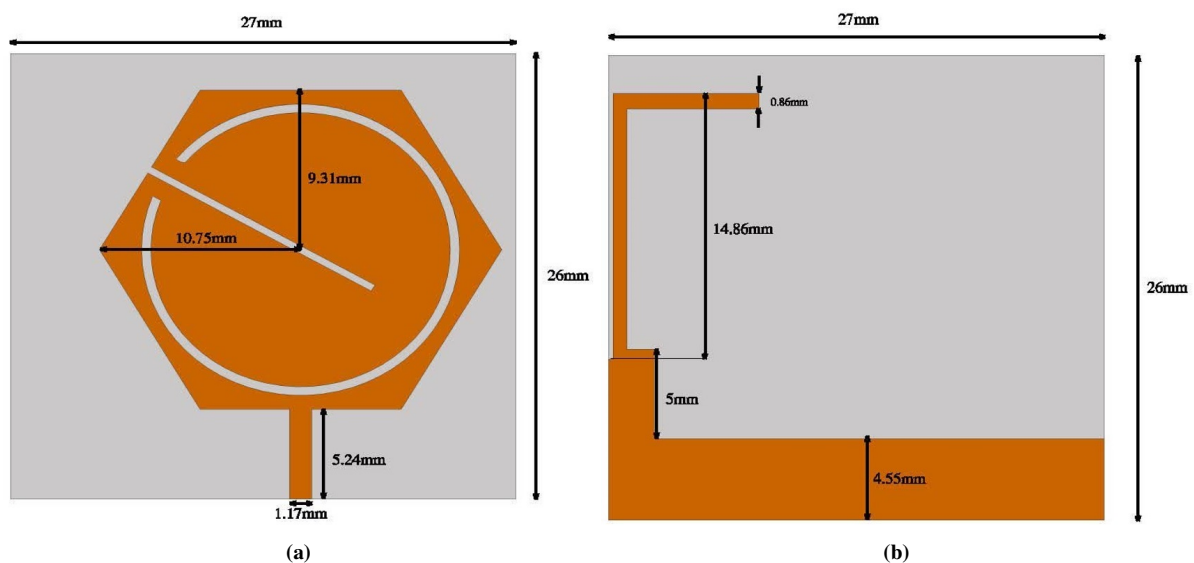


Figure 1. The Microstrip antenna, (a) top view, (b) bottom view.

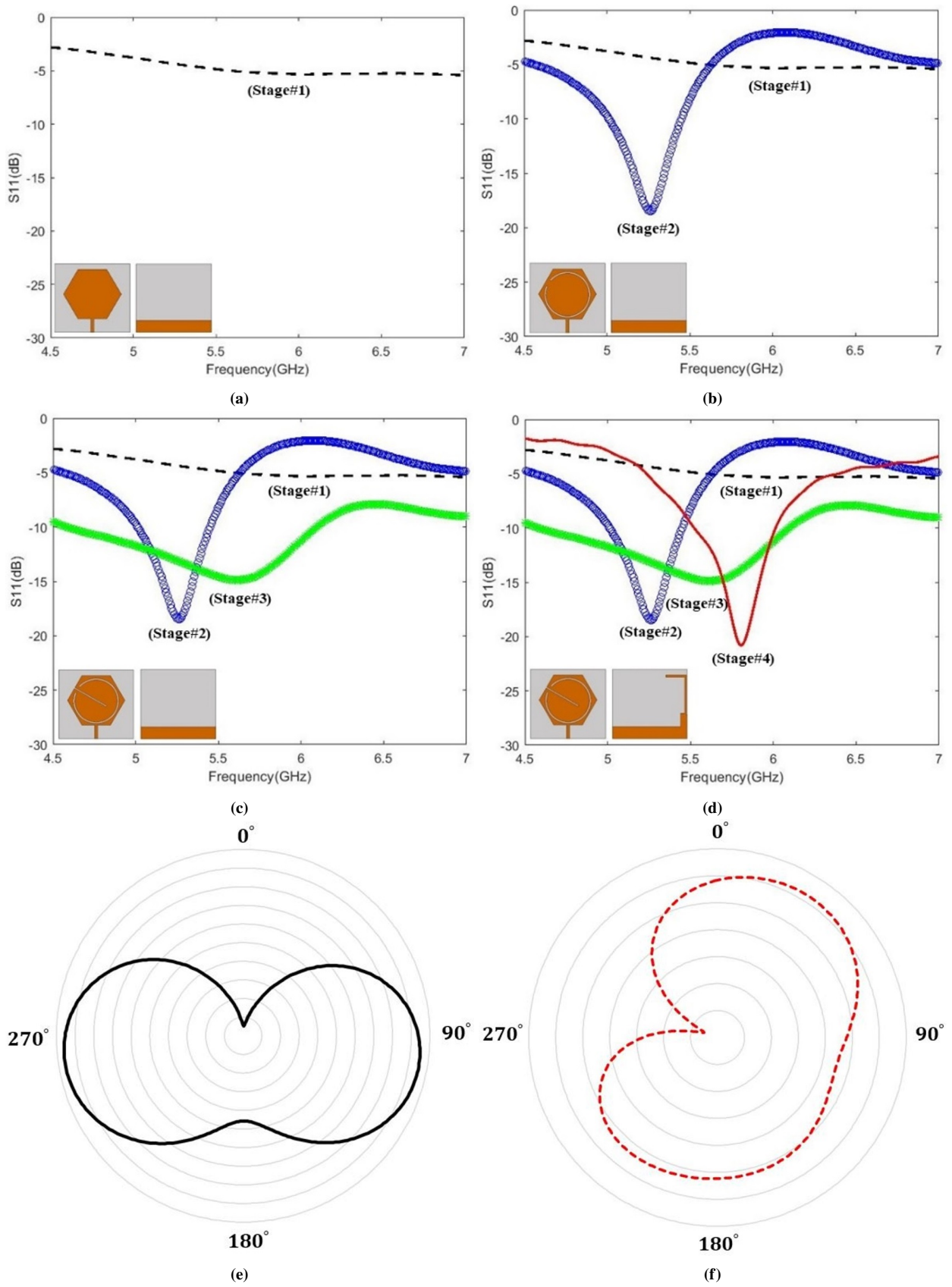


Figure 2. The single-element antenna design steps with related S_{11} diagram (a) step#1, (b) step#2, (c) step#3, (d) step#4, simulated far-field pattern at 5.8 GHz (e) H-plane (f) E-plane.

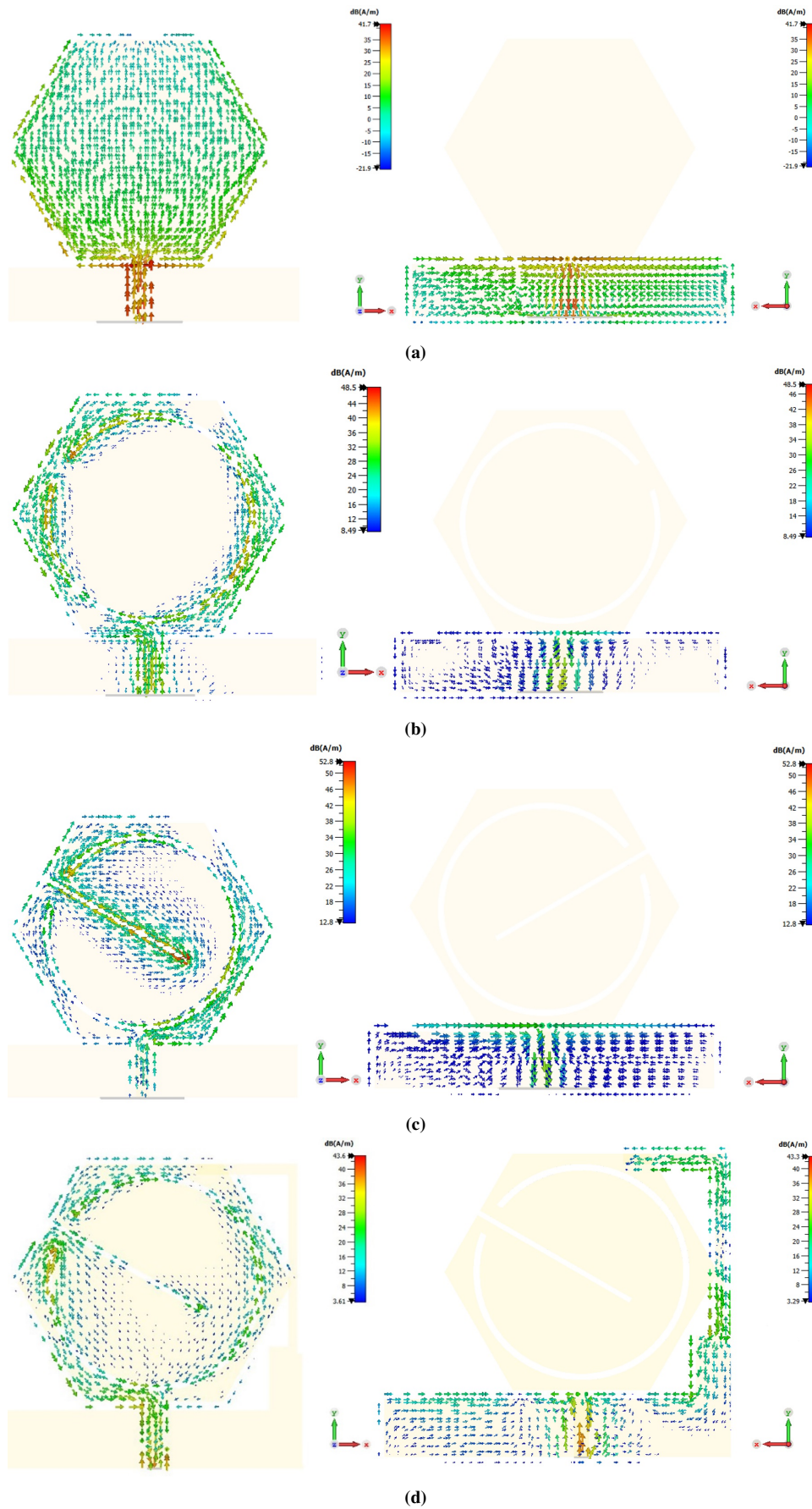


Figure 3. Distribution of surface current at 5.8 GHz (a) step#1, (b) step#2, (c) step#3, (d) step#4.

$$W = \frac{c}{2f_r} \sqrt{\frac{2}{\varepsilon_r + 1}} \quad (1)$$

where c is the velocity of light, f_r is the resonant frequency and ε_r is the dielectric constant of substrate.

$$L = L_{eff} - \Delta L \quad (2)$$

where L_{eff} is effective length of the patch given as follows:

$$L_{eff} = \frac{c}{2f_r \sqrt{\varepsilon_{eff}}} \quad (3)$$

and ΔL is the extended incremental length given as follows:

$$\Delta L = 0.412h \frac{(\varepsilon_{eff} + 0.3) \left(\frac{w}{h} + 0.264\right)}{(\varepsilon_{eff} - 0.258) \left(\frac{w}{h} + 0.8\right)} \quad (4)$$

where ε_{eff} is the effective dielectric constant given as follows:

$$\varepsilon_{eff} = \frac{\varepsilon_r + 1}{w} + \frac{\varepsilon_r - 1}{w} \left(1 + \frac{12h}{w}\right)^{-\frac{1}{2}} \quad (5)$$

Table 1 presents the calculated dimensions of the proposed patch antenna, which were derived using equations (1)-(5). These dimensions have been adjusted using CST Microwave Studio to improve the overall performance of the antenna for operation at 5.8 GHz, as illustrated in figure 1.

3. Analysis results of microstrip MIMO array

The designed and fabricated sample of the top/bottom of a proposed MIMO structure is presented in Figs. 4 and Figs. 5, respectively, which consists of double microstrip antennas arranged next to one another in a mirror pattern.

According to Figs. 6 (a,b), the bandwidth of this MIMO antenna obtained 13.79% (5.4 – 6.2 GHz), and isolation is more than 22 dB ($S_{21} \leq -22$ dB), which caused optimal performance.

The photograph of the manufactured MIMO antenna prototype in the anechoic chamber is presented in figure 7. Figures 8 (a,b) are the simulated radiation patterns on the H-plane and E-plane of the proposed microstrip MIMO radiator at 5.8 GHz. The peak gain and efficiency have obtained 5 dB and 95%, respectively. The overall simulation and measurement outcomes of the MIMO

array have an appropriate overlap, however, due to the fabrication faults and different conditions, some mismatches have occurred between results. Figures 8 (c-f) demonstrate simulated radiation patterns on both the H-plane and E-plane of the proposed microstrip MIMO far-field pattern at 5.4 GHz and 6.2 GHz. Figure 8 (d) presents the antenna gain over its operational frequency range. According to the data, the antenna gains at 5.2, 5.8, and 6.2 GHz are 4.9, 5, and 4.8 dB, respectively. In the MIMO configuration, the ground planes of the antenna elements are merged and expanded to create a unified structure. Consequently, it is expected that the radiation pattern shown in Fig. 8 (b) will exhibit slight differences compared to the single-element case presented in Fig. 2 (f).

3.1 MIMO specifications

To legitimize the proposed antenna specifications as a MIMO antenna, numerous parameters for example channel capacity reduction (CCL), mean effective gain (MEG), envelope correlation coefficient (ECC), and diversity gain (DG) should be considered. All the MIMO antenna parameters have been investigated according to the S-parameters.

3.2 ECC and DG parameters

ECC can estimate the correlation and isolation between MIMO antenna elements [42]. According to the third-generation partnership project (3GPP) industrial standard, to keep an optimal implementation of a MIMO antenna, the ECC value is necessary to be below 0.5, so that each element antenna can function independently, without affecting another element [43]. The simulated and measured ECC is calculated using equation (6), with scattering parameter values [13]. Figure 9 (a) illustrates ECC, which is below 0.02 for all 5.4 – 6.2 GHz bandwidth.

$$ECC = \frac{|S_{11}^* S_{12} + S_{21}^* S_{22}|}{(1 - |S_{11}|^2 - |S_{21}|^2)(1 - |S_{22}|^2 - |S_{12}|^2)} \quad (6)$$

In the MIMO antenna, diversity gain describes the obtained gain from multiple antennas in comparison to the singular element. Regularly a DG standard must be about 10 dB [44]. According to equation (7), the ECC of a MIMO array can be used to determine DG [45]. Figure 9 (a) shows that DG is close to 10 dB over the

Table 1. Dimensions of the patch antenna.

	Dielectric constant of substrate ε_r	Thickness of substrate (mm)	Effective dielectric constant ε_{eff}	Patch Width (mm)	Patch length (mm)	Extended incremental length ΔL (mm)
Original Value equations (1)-(5)	3.38	0.508	3.21	17.48	13.93	0.245
Modified Values (CST Microwave Studio)	3.38	0.508	3.24	21.5	18.62	0.248

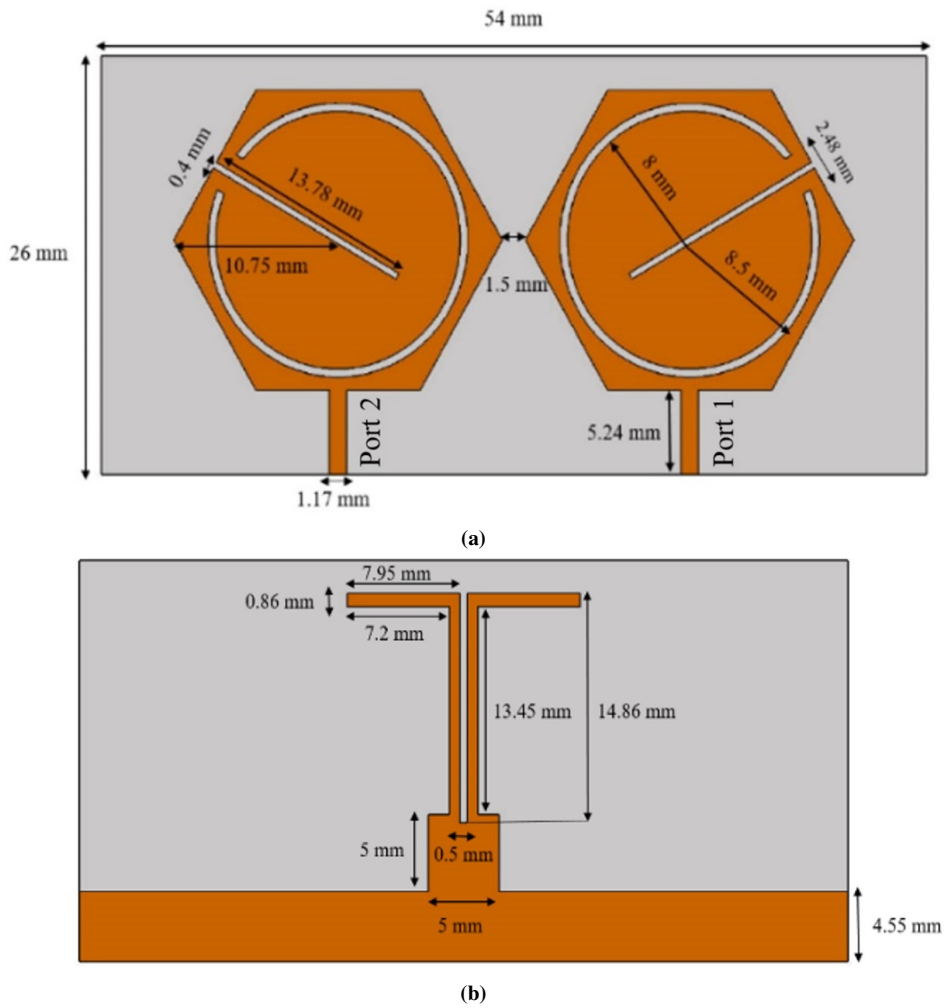


Figure 4. The proposed microstrip MIMO array with designed details: (a) top view, (b) bottom view.

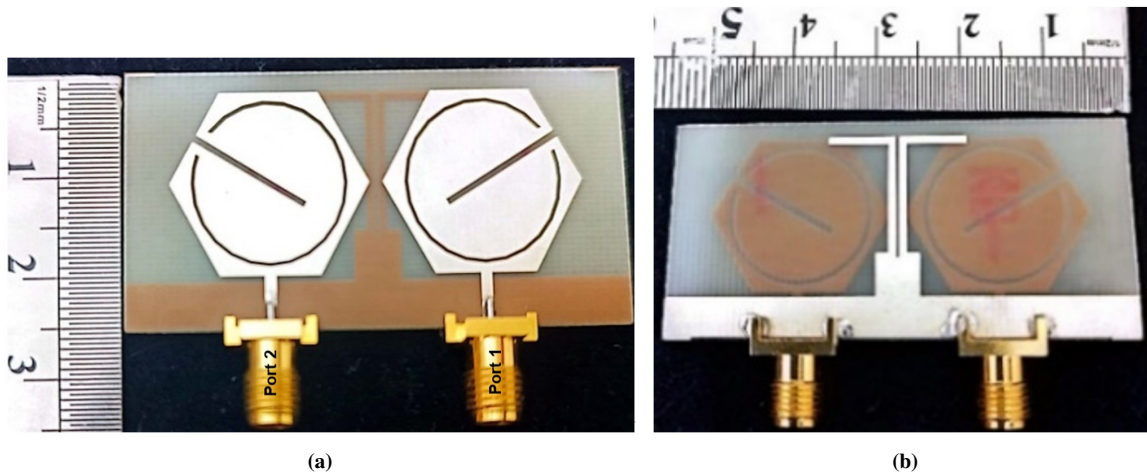


Figure 5. The photographs of fabricated prototype microstrip MIMO array: (a) top photo, (b) bottom photo.

operating range.

$$DG = 10\sqrt{1 - ECC^2} \quad (7)$$

3.3 CCL parameter

Channel capacity can be expressed based on Shannon’s theorem, which is an extreme possible information transfer rate through a communication channel without any

interference. As a result, the system performance decline can be measured in CCL terms. The acceptable CCL values for MIMO systems are lower than 0.4 b/s/Hz. The CCL results are presented in Fig. 9 (b), which are below 0.2 b/s/Hz for the entire operational bandwidth. The CCL can be explained by equation (8), where β^R is an

antenna correlation matrix [46, 47]:

$$CCL(LOSS) = -\log_2 \det \beta^R \tag{8}$$

where

$$\beta^R = \begin{bmatrix} R_{ii} & R_{ij} \\ R_{ji} & R_{jj} \end{bmatrix} \tag{9}$$

$$R_{ii} = 1 - (|S_{ii}|^2 + |S_{ij}|^2) \tag{10}$$

$$R_{ij} = - (S_{ii}^* S_{ij} + S_{ji}^* S_{jj}) \tag{11}$$

3.4 MEG parameter

In the MIMO antenna with multipath fading situation, MEG compares the power that is given by a multiple antenna to an isotropic antenna obtained power. Matching

power level, the ratio between MEGs (MEG₁/MEG₂) ought to be less than 3 dB [48]. Figure 9 (c) shows the ratio between MEGs which is 1 dB, within the standard range. MEGs can be estimated using equations (12) and (13), where $\eta_{1,rad}$ and $\eta_{2,rad}$ are the radiation coefficients in port 1 and 2, which are calculated by S-parameters for MEG₁ and MEG₂, respectively [49]:

$$MEG_1 = 0.5\eta_{1,rad} = 0.5 [1 - |S_{11}|^2 - |S_{12}|^2] \tag{12}$$

$$MEG_2 = 0.5\eta_{2,rad} = 0.5 [1 - |S_{12}|^2 - |S_{22}|^2] \tag{13}$$

The IoT is a vast integrated network that enables the exchange of large amounts of data at high speeds. IoT is recognized for its affordability, intermediate data rates, and an operating frequency range between 100 MHz

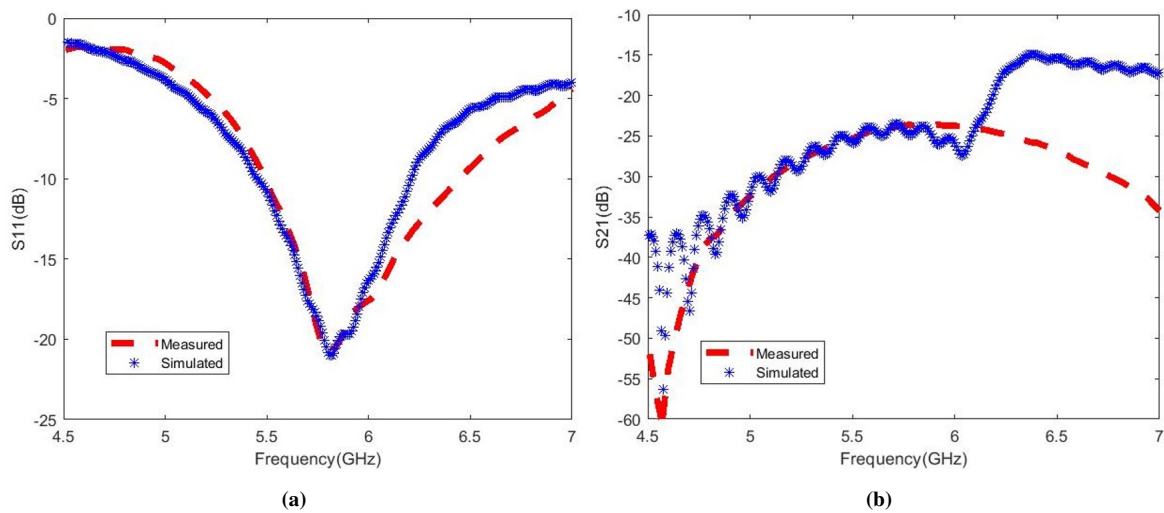


Figure 6. Measured and simulated (a) S_{11} and (b) S_{21} parameters of MIMO antenna.

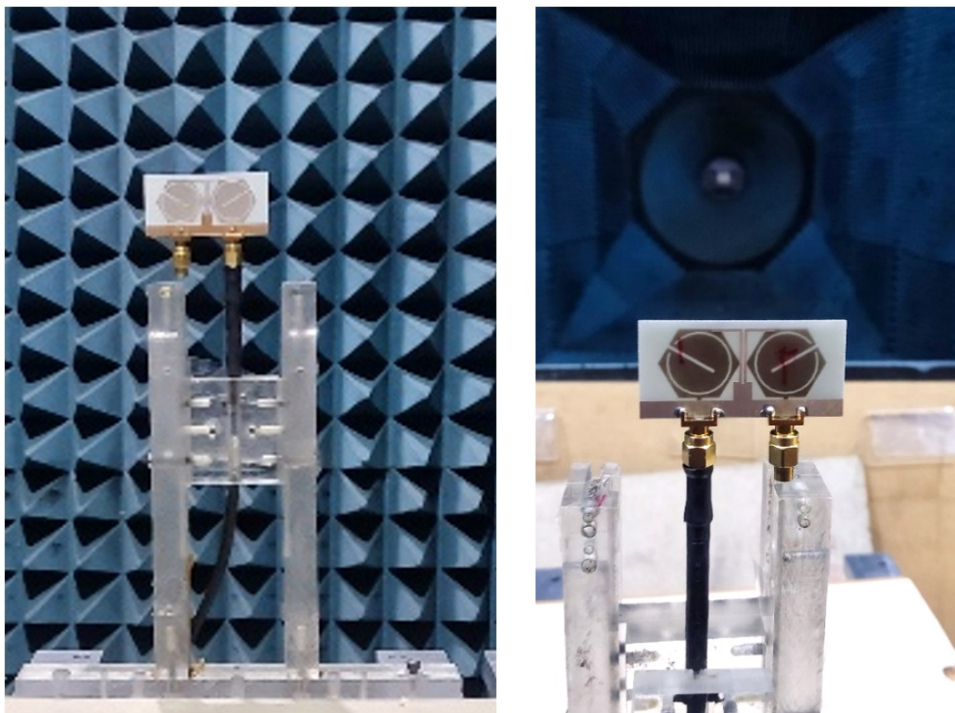


Figure 7. The photograph of the fabricated prototypes of the MIMO antenna under test in anechoic chamber.

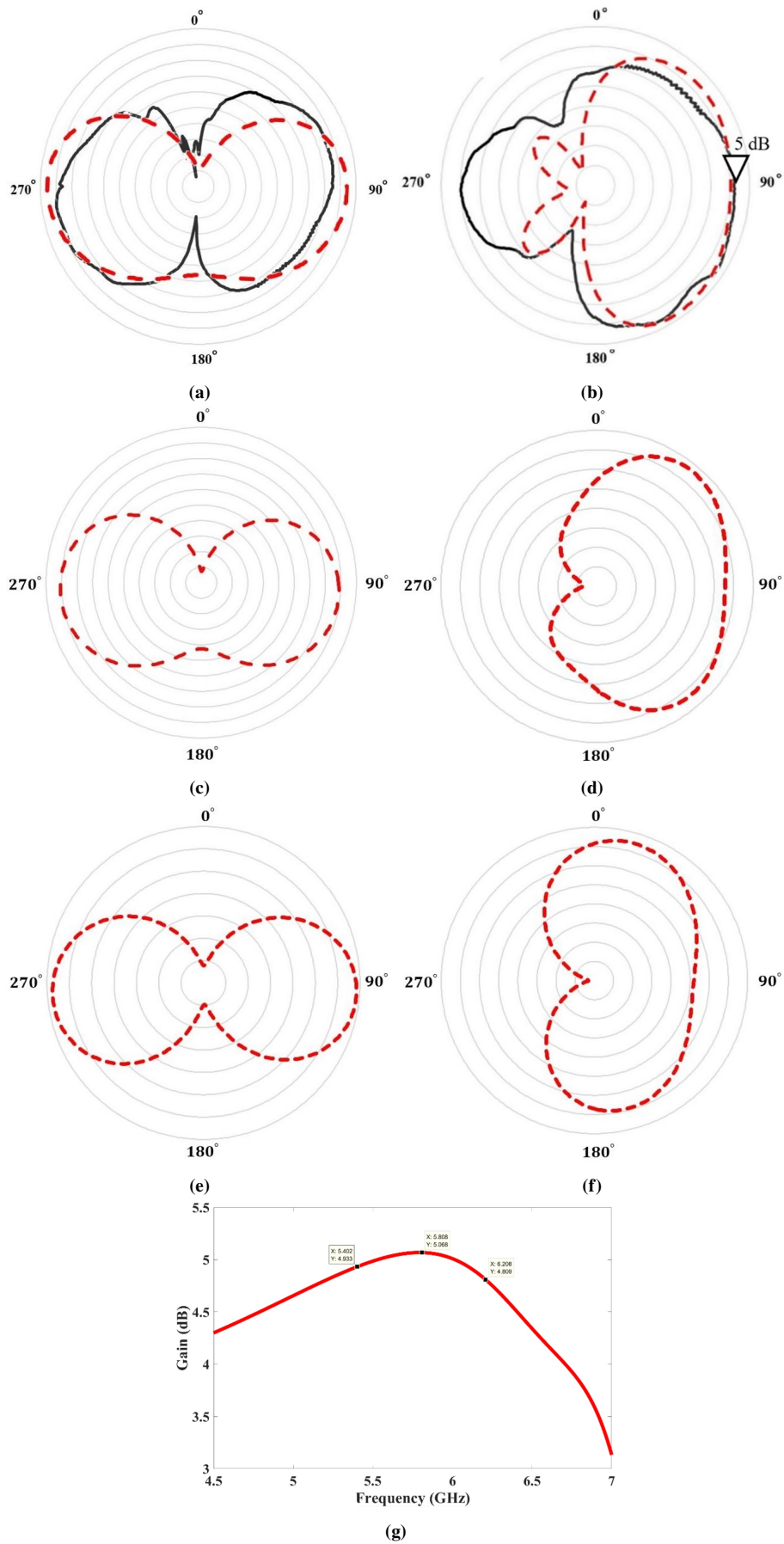


Figure 8. Measured and simulated (a) H-plane, (b) E-plane far-field pattern at 5.8 GHz, simulated of far-field pattern at 5.4 GHz (c) H-plane, (d) E-plane, and simulated of far-field pattern at 6.2 GHz (e) H-plane, (f) E-plane, (g) Diagram of antenna gain across the frequency range covered.

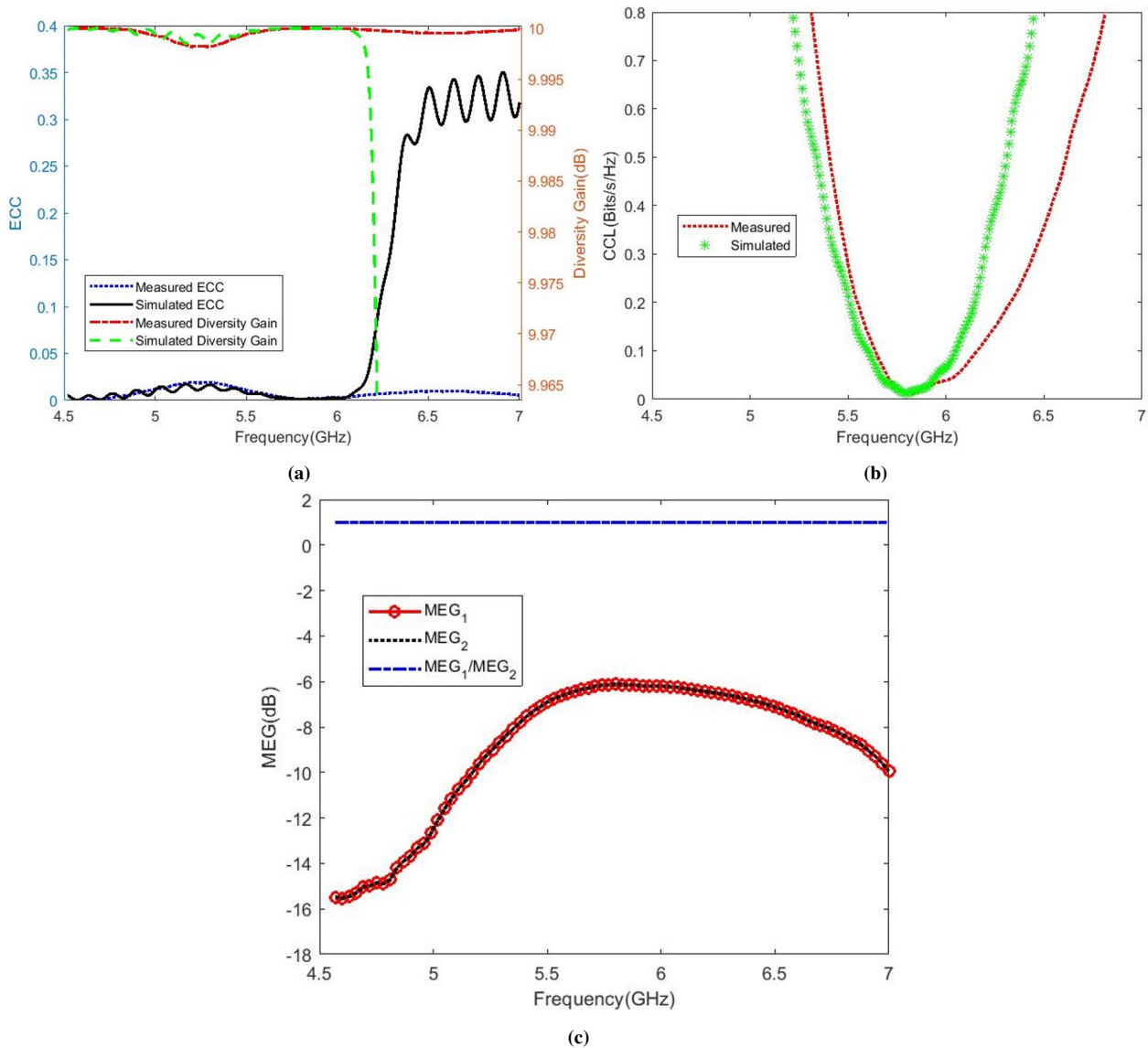


Figure 9. The proposed MIMO antenna diversity parameter (a) measured/simulated DG and ECC, (b) measured/Simulated CCL, (c) simulated MEGs.

and 5.8 GHz. IoT applications do not require specific bandwidth when operating at a frequency of 5.8 GHz [70]. The ISM band technology is primarily utilized in various applications. One of the frequency ranges available for ISM applications is 5.725 to 5.875 GHz [71, 72]. Therefore, the proposed antenna operating within a frequency range of 5.8 to 6.2 GHz with high gain and efficiency is suitable for ISM and IoT applications.

Table 2 presents a comparison of the proposed MIMO antenna with results from similar studies. The analysis reveals that the proposed antenna exhibits excellent efficiency when compared to references [51], [64], and [66]. It also demonstrates good gain relative to [42], [60], and [62]. Furthermore, in terms of isolation, it is comparable to studies [11], [63], and [65]. Consequently, the proposed MIMO antenna stands out as a suitable option for ISM/IoT applications due to its compact size, impressive gain, and high efficiency.

4. Conclusions

This study presents an original 2×1 microstrip MIMO array antenna for frequencies range between 5.4 GHz and 6.2 GHz, achieving a fractional bandwidth of 13.79%. The planned MIMO array is constructed with double mirror elements on a Rogers 4003C board, with dimensions of $54 \times 26 \times 0.508 \text{ mm}^3$. The outcomes of the proposed antenna demonstrate a peak gain of 5 dB and an efficiency of 95% at 5.8 GHz frequency. Additionally, the specifications of this design have been compared with various similar works. According to these comparisons, this antenna is appropriate for ISM/IoT applications.

Table 2. Performance comparisons between different parameters of the proposed microstrip MIMO antenna with previous works.

Ref.	Frequency (GHz)	Bandwidth % (GHz)	Dimension (mm ³)	Gain (dB)	Efficiency (%)	Isolation (dB)	Application(s)
[8], 2022	2.4 3.5 5.5	8 (2.28–2.47) 11 (3.34–3.73) 38 (4.57–6.75)	0.56 × 0.36 × 0.018	1.3 2.9 4.3	–	20	ISM, 5G, WLAN
[42], 2021	2.4 6.5	87 (3–7.7)	0.37 × 0.25 × 0.006	3	78	20	Wireless
[43], 2021	3.7	24 (3.3–4.2)	0.45 × 0.36 × 0.009	2.5	95	15	5G
[50], 2020	5.8	2 (5.72–5.89)	1.07 × 0.87 × 0.029	5.36	–	20.19	Wireless
[51], 2019	2.6	29 (2.16–2.92)	0.34 × 0.19 × 0.013	7.02	82.1	14.5	Small Satellite
[52], 2018	5.5	11 (5.25–5.92)	1.10 × 0.73 × 0.157	5	90	20	WLAN
[53], 2020	2.46	2.83 (2.43–2.5)	0.76 × 0.30 × 0.012	4.25	77.81	24.67	WLAN
[54], 2020	5.8	3.44 (5.7–5.9)	1.06 × 1.06 × 0.309	5.3	84	32	WLAN, LTE
[55], 2020	6.44	35 (5.71–8.2)	1.70 × 1.70 × 0.106	3.8	80	15	C-band
[56], 2022	2.45	25 (2.15–2.77)	0.04 × 0.03 × 0.00096	-22.7	–	30.1	Wireless capsule
[57], 2022	6	3 (5.9–6.1)	0.80 × 0.64 × 0.02	5.2	73	40	5G
[58], 2022	4	46 (3.12–5)	0.33 × 0.26 × 0.021	2.5	70	18.5	5G
[59], 2022	3.38 4.78	18.3 (2.99–3.61) 8.1 (4.53–4.92)	0.68 × 0.28 × 0.016	3.05 3.76	74.46 84.93	25 16	5G
[60], 2023	5.37	2 (5.3–5.46)	0.68 × 0.56 × 0.017	4.54	74	51.5	–
[61], 2023	5.4	10.8 (5.25–5.85)	1.43 × 0.89 × 0.014	6.5	90	25	WLAN
[62], 2023	2.5 4.5	6 (2.40–2.57) 57 (3.85–6.96)	0.37 × 0.25 × 0.006	2.65	70	15	5G, Wi-Fi
[63], 2023	3.7–7.7	112 (2.9–10.4)	0.43 × 0.30 × 0.019	5	90	20	IoT, Wearable
[64], 2022	5.8	4 (5.65–5.9)	0.48 × 0.99 × 0.03	5.6	93	17-30	WLAN
[65], 2022	2.4 5.56	12.7 (2.2–2.5) 10.7 (5.2–5.8)	1.40 × 0.80 × 0.012	–	28 16.2	20	Wi-Fi
[66], 2025	3.5 5.8	(3.01-6.5)	0.77 × 0.77 × 0.018	7.66 7.74	71.5	20	5G, WiMAX
[67], 2024	2.4	20.8 (2.2-2.7)	0.128 × 0.048 × 0.002	2.3	5.41	34	IoT
[68], 2023	3.5 6	35.7 (3.45 – 4.7) 36.6 (5.6-7.8)	0.6 × 0.41 × 0.021	1 3.8	87 85	17 26	5G, WLAN
[69], 2023	5.8	3.4 (5.7-5.9)	0.65 × 0.56	3.55	65	25	5G, IoT
Proposed	5.8	13.79 (5.4–6.2)	1.04 × 0.50 × 0.0098	5	95	22	ISM, IoT

Acknowledgment

This research is funded by Semnan University, research grant 1403942. The authors would like to thank all the members of antenna laboratory at Iran Telecommunication Research Center (ITRC), for their cooperation. Also, the authors would like to thank the Editor and reviewers for their constructive comments.

Authors contributions

All authors contributed equally to the conception, design, execution, and writing of this work. All authors read and approved the final manuscript.

Availability of data and materials

The authors declare that the data supporting the findings of this study are available within the paper.

Conflict of interests

The authors assert that they do not have any identifiable conflicting financial interests or personal relationships that might be perceived to influence the work presented in this paper.

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