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# Effects of strontium and copper substitution on the catalytic performance of LaCoO<sub>3</sub> in the combustion of methane: an optimization study

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#### ABSTRACT

Cobalt-based perovskites containing strontium and copper ( $La_{1-x}Sr_xCo_{1-y}Cu_yO_3$ ) were synthesized by the sol-gel method and characterized by XRD, H<sub>2</sub>-TPR, N<sub>2</sub>-adsorbtion, XRF and XPS techniques. The XRD results showed that the rhombohedral structure of perovskites was obtained. The activation energy employed to analyze the activities of samples in the combustion of methane was optimized using full factorial design (FD) by considering strontium (x=0, 0.1 and 0.2) and copper (y=0, 0.25 and 0.5) as the input variables. Analysis of Variance (ANOVA) was employed to investigate the obtained data and a p<0.05 was considered statistically significant. A second-order quadratic model was developed to calculate the activation energy on the basis of strontium and copper doping-degrees. FD results showed that perovskites containing strontium and copper in the range of 0.07-0.15 and of 0.2-0.4, respectively, had the best catalytic activity owing to the higher surface area, higher amounts of oxygen species, better reducibility and oxygen mobility.

Keywords: Methane, Perovskite, Cobalt, Strontium, Copper

#### **1.Introduction**

Methane presents at low concentrations in many fugitive emissions, such as car exhaust gases, and needs further process to prevent pollution. Catalytic combustion is the main process for oxidation of unburned methane. As compared to conventional flame combustion, it needs lower temperatures and accordingly leads to lower emissions of CO and NOx. Since, conventional flame combustion uses temperatures as high as 1800 °C, a high amount of nitrogen oxides  $(NO_x)$  will be formed [1, 2]. Although supported palladium oxide is known to be a very active catalyst for catalytic conversion of hydrocarbons, its application has been limited because of sinterization and deactivation problems. It has been reported that sintering of Pd particles is significant only at 600 °C or above [3]. Furthermore, the high cost of Pd is another obstacle which should be considered [4, 5]. Perovskites are mixed oxides of general formula ABO<sub>3</sub>,

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where A and B are mainly rare earth and transition metal cations respectively [5, 6]. Both A and B can be partially substituted by different kinds of rare earth and transition metals to make perovskite-type oxides of general formula  $A_{1-x}A_xB_{1-y}B_yO_3$  [4, 5]. In Perovskite materials, activity is related to B while A is responsible for the formation of crystal lattice and its stability. However, when A is partially substituted by A', it affects the valence state of B which can improve the catalytic activity [4, 7]. Perovskite-type oxides have attracted scientists' attention and are considered as potential substitutes due to high thermal stability and activity.

Among different types of perovskite materials, LaCoO<sub>3</sub> has attracted more attention due to its specific oxygen nonstoichiometries which can be further modified through the partial substitution of A- or B-site metal ions [6, 8-10]. Many efforts have been made to increase LaCoO<sub>3</sub> activity by partial substitution of lanthanum (La) and cobalt (Co) cations [8, 9, 11]. The addition of Cu into LaCoO<sub>3</sub> increased its activity in the reduction of NO by CO [12]. Glisenti et al. [13] reported that oxidation ability of LaCoO<sub>3</sub> was noticeably

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better than that of LaCoO<sub>3</sub>. Moreover, our previous study demonstrated that incorporation of Ni. Cu and Fe into LaCoO<sub>3</sub> increased its catalytic activity in combustion of methane [14]. Partial substitution of Co cations by transition metals such as Cu can change the valency of Co cations and accordingly modify the oxygen mobility and reducibility [9, 15]. For instance, oxygen vacancies can be formed through substituting trivalent Co cation ( $Co^{3+}$ ) by a bivalent cation (such as  $Cu^{2+}$ ) due to positive charge deficiencies. Strontium (Sr) is reported as an appropriate candidate to be partially substituted at La sites. For instance, Kim et al. [16] reported that La<sub>0.9</sub>Sr<sub>0.1</sub>CoO<sub>3</sub> and La<sub>0.9</sub>Sr<sub>0.1</sub>MnO<sub>3</sub> perovskites had higher NO oxidation activity than Ptbased catalysts. Zhang et al. [17] found that the addition of Strontium into La<sub>2</sub>CuO<sub>4</sub> increased its performance in methane oxidation.

According to the literature [9, 15, 17], the addition of Strontium into cobalt based perovskites results in an improvement in catalytic oxidation reactions. Partial substitution of Sr<sup>+2</sup> at La<sup>+3</sup> sites in LaCoO<sub>3</sub> lattice creates a net charge imbalance that needs to be compensated by oxygen vacancies to keep the charge balanced .It has been found that reducibility and oxygen mobility improved by this phenomenon. On the other hand, recent researches have shown that Cu can make impressive effects on the oxygen mobility of LaCO<sub>3</sub>. When Co is partially substituted by Cu, the structure of  $LaCoO_3$  has to be distorted which causes the appearance of some anionic deficiencies. This phenomenon leads to some transformation in the valence states of Co cations, resulting in the improvement of the catalytic behavior [12, 18].

Consequently, different types of La<sub>1-x</sub>Sr<sub>x</sub>Co<sub>y</sub>Cu<sub>1-y</sub>O<sub>3</sub> perovskites were synthesized to study the effects of Sr and Cu metals on the catalytic properties of LaCO<sub>3</sub>. For this purpose, the experimental design of experiments (DoE) was employed to investigate interaction effects of Sr and Cu. The potential for using DoE in data analysis is especially high in the case of systems with nonlinear and interaction effects because DoE possesses the capability to be developed from a set of experimental data without actual knowledge of the physical and chemical laws that govern the system [19, 20]. In this study, nine cobalt-based perovskite-type oxides were synthesized with different amounts of Sr and Cu. The obtained solids were characterized by XRD, BET, H<sub>2</sub>-TPR XPS techniques to investigate and physicochemical properties of them. Finally, full factorial design of experiments coupled with response surface methodology were employed to investigate the effects of Sr and Cu on the combustion of methane and optimize Sr and Cu doping degrees in LaCoO<sub>3</sub> lattice.

#### 2. Experimental

#### 2.1. Catalyst preparation

 $La_{1-x}Sr_xCo_{1-y}Cu_yO_3$  perovskites with x=0, 0.1, 0.2 and y=0, 0.25, 0.5 were synthesized by the citric acid sol-gel method using  $La(NO_3)_3.6H_2O_1$ ,  $Co(NO_3)_2.6H_2O_1$ ,  $Cu(NO_3)_2 \cdot 3H_2O$ ,  $Sr(NO_3)_2$ , citric acid  $(C_6H_8O_7)$  and ethylene glycol ( $C_2H_6O_2$ ) as the starting materials [12, 21, 22]. All starting synthesis grade materials were supplied by Merck Company. Briefly, appropriate quantities of citric acid, ethylene glycol and a little amount of water were mixed with vigorous stirring to obtain a homogeneous viscous solution. Then, Stoichiometric quantities of Co(NO<sub>3</sub>)<sub>2</sub>.6H<sub>2</sub>O and  $Cu(NO_3)_2 \cdot 3H_2O$  were added to the solution and allowed to stir at 65 °C until a clear solution was obtained. Afterward, stoichiometric amounts of La(NO<sub>3</sub>)<sub>3</sub>.6H<sub>2</sub>O and Sr(NO<sub>3</sub>)<sub>2</sub> were added and allowed to stir at 65 °C until the excess solvents evaporated and a spongy gel was formed. In the next step, the spongy gel was dried at 65 °C for 24h in an oven and finally calcined at 800 °C in the air for 4h.

For all samples, the molar ratios of citric acid/ethylene glycol/total nitrates were kept at 5:5:1 while the molar ratios of total A ions (La+Sr) to total B ions (Co+Cu) were kept at 1:1. The synthesized samples were labeled as SrxCuy where x refers to Sr and y refers to Cu. For instance,  $La_{0.9}Sr_{0.1}Co_{0.5}Cu_{0.5}O_3$  was labeled as Sr0.1Cu0.5. The composition of the initial gels for all synthesized samples are given in **Table 1**.

#### 2.2. Catalyst characterization

X-ray diffraction studies were performed using an 1840 Philips diffractometer with Cu K $\alpha$  radiation ( $\lambda = 1.54$  Å) in the 2 $\theta$  range of 20–80 with a step size of 0.02 °/s, to investigate the structure and crystallinity of the samples. The operating voltage and current were 40 kV and 40 mA, respectively.

The surface area and pore volume of the samples were measured by Nitrogen adsorption and desorption experiments at -196 °C using a Micromeritics TriStar 3000 automated system. Before experiments, the samples were first degassed for 2 h at 200 °C to remove moisture. The surface area was calculated by the BET method. X-ray fluorescence (XRF) technique using a Philips PW2404 XRF spectrometer was employed to analyze the elemental composition of the samples.

To investigate the chemical bonding state of the desired elements, X-ray photoelectron spectroscopy (XPS) tests were carried out on a Gammadata-scienta ESCA 200 hemispherical analyzer using an Al K $\alpha$  (1486.6 eV) X-ray source.

 Table 1. Coded and actual values of the variables of the design of experiments

Factor	Variable	Level		
		-1	0	1
А	Cu doping degree (at%)	0	0.25	0.5
В	Sr doping degree (at%)	0	0.1	0.2

The spectra were registered after degassing the samples at ambient temperature under vacuum. The electron binding energies were calibrated by the C 1s hydrocarbon peak at 285 eV as a reference.

Reduction reactivity of the samples was investigated using hydrogen temperature-programmed reduction analysis (H<sub>2</sub>-TPR) by a Micrometer 2900 equipped with a thermal conductivity detector (TCD). Each sample was weighted 50 mg and was loaded into a tubular quartz microreactor. The sample was first purged at 300 °C for 1h under a flow of Ar and then cooled to room temperature. Then, H<sub>2</sub>-TPR step was conducted in a reducing gas flow of 10% H<sub>2</sub> in Ar with concomitant temperature leveling up to 900 °C with a heating rate of 10 °C /min.

#### 2.3. Evaluation of catalytic performance

Catalytic experiments for the combustion of methane were performed in a fixed bed quartz reactor with an internal diameter of 10 mm and 50 cm length at a temperature ranging from 350 °C to 750 °C under atmospheric pressure. A schematic representation of the set-up is shown in **Scheme 1**.

For all tests, 200 mg catalyst was taken and loaded into the reactor. The total flow rate of the reactant gas with a molar composition of  $CH_4:O_2:N_2 = 2:18:80$  was equal to 30 cm<sup>3</sup>/min which was controlled by mass flow controllers. The gas phase effluent from the reactor was analyzed online using a Varian CP-3800 gas chromatograph equipped with a flame ionization detector (FID) and a thermal conductivity detector (TCD). The apparatus employed CP-Sil 5CB column and Molsieve 13c to separate the desired components. The activation energy (E) was employed to compare the catalytic activities of the samples.

Calculations of the activation energies were done by assuming a simple first-order reaction rate. Hence, the  $ln(-ln(1 - \alpha)) = (1000/RT)$  dependence was plotted where  $\alpha$ , T and R are the conversion of methane, temperature and gas constant, respectively. The activation energies were calculated by the Arrhenius equation based on the slope of the plotted straight line [23, 24].

2.4. Statistical method and data analysis

Effects of Sr and Cu as independent variables on activation energy in the catalytic combustion of methane were investigated using full factorial design of experiments. These variables were identified at three different levels of 0, 0.1 and 0.2 for Sr and 0, 0.25 and 0.5 for Cu. The values were selected based on the results of preliminary experiments. Three factorial levels for each variable were coded as -1, 0 and +1 for low, medium and high using **Eq. (1)** [19, 20].

Where  $x_i$  is the coded value of *ith* factor,  $X_i$  is the actual value of *ith* factor,  $X_0$  is the actual value of  $X_i$  at the medium point and  $\Delta X_i$  is the factor-variation interval. The independent variables with their values in actual and coded form are given in **Table 2**.

In a full factorial design for two variables, a total of 9 runs were required which can be determined using **Eq.** (2).

$$n_e=3^k$$
 (2)

Where  $n_e$  is the total number of experiments and k is the number of independent variables. Behavior of the system as a function of independent variables in this study was expressed by the following second-order polynomial equation:

$$Y = \beta_0 + \sum_{i=1}^k \beta_i X_i + \sum_{i=1}^k \beta_{ii} X_i^2 + \sum_{i=1}^k \sum_{i$$

Where Y is the predicted response, k is the number of independent parameters,  $\beta_0$  is an intercept coefficient,  $\beta_i$  is a linear term,  $\beta_{ii}$  is a quadratic term,  $\beta_{ij}$  is an interaction term and  $X_i$  and  $X_j$  are the actual variables.



Scheme 1. Schematic representation of the set-up

sample	sample Cell volume BET surface area Pore (A <sup>3</sup> ) $(m^2/g)$ volume $(cm^3/g)$	Pore	Bulk compositiona (at%)				
		$(cm^3/g)$	La	Sr	Со	Cu	
LaCoO <sub>3</sub>	338.26	9.8	0.09	52.1 (50) <sup>a</sup>	0	47.9 (50)	0
Sr0Cu0.25	339.28	9.1	0.08	51.8 (50)	0	35.4 (37.5)	12.8 (12.5)
Sr0.1Cu0.25	339.32	8.7	0.08	40.8 (40)	9.7 (10)	35.1 (37.5)	14.4 (12.5)
Sr0.2Cu0.25	339.84	7.9	0.06	32.5 (30)	18.2 (20)	35.9 (37.5)	13.4 (12.5)
Sr0.1Cu0	338.37	10.1	0.09	42.3 (40)	9.5 (10)	48.2 (50)	0
Sr0.1Cu0.50	342.56	6.7	0.06	41.8 (40)	9.1 (10)	21.76 (25)	27.34 (25)

Table 2. Physical properties and bulk composition of the perovskites

<sup>a</sup> Nominal values are in parentheses.

#### 3. Result and Discussion

#### 3.1. Catalyst characterization

#### 3.1.1. XRD

**Fig. 1** presents the XRD results of the  $La_{0.9}Sr_{0.1}Co_{1-}$  $_{v}Cu_{v}O_{3}$  (Fig. 1a) and  $La_{1-x}Sr_{x}Co_{0.75}Cu_{0.25}O_{3}$  (Fig. 1b) samples. As a reference, the XRD pattern of LaCoO<sub>3</sub> is given in both Fig. 1a and Fig. 1b. According to Fig. 1a, XRD characterization revealed that all La<sub>0.9</sub>Sr<sub>0.1</sub>Co<sub>1-</sub>  $_{v}Cu_{v}O_{3}$  samples possessed reflex ions ascribed to the rhombohedral LaCoO<sub>3</sub> structure (JCPDS card 48-0123). No diffraction peaks related to impurity oxides were observed in Sr0.1Co0 and Sr0.1Co0.25 samples, indicating the formation of the perovskite structure with single phase. However, a trace amount of segregated Cu oxide phases could be detected in the XRD pattern of Sr0.1Co0.5 sample. Later as demonstrated by XPS, a large amount of Cu exited with the oxidation state of Cu<sup>+2</sup> in the perovskite structure. This phenomenon is attributed to the fact that the ionic radius of Cu<sup>+2</sup> is larger than Co+3, resulting in the segregation of some CuO when its amount was high [12, 25]. It should be noted that the intensity of the peaks of the X-ray diffraction patterns decreased as the amount of Cu increased which demonstrates the grain size became smaller and crystallinity fallen. Furthermore, the main diffraction peak at  $2\theta = 33^{\circ}$  shifted slightly toward the lower angles as more Cu was substituted at Co sites, indicating the appearance of the lattice expansion because of the larger ion radius of  $Cu^{+2}$  as compared to  $Co^{+3}$  [26]. This can also be seen from the cell volume size in Table 3.

**Fig. 1b** shows that the perovskites with the rhombohedral structure were formed for all  $La_{1-x}Sr_xCo_{0.75}Cu_{0.25}O_3$  samples without any impurities. The main characteristic peak around 33° slightly shifted toward higher angles and its intensity decreased as Sr substitution degree increased, indicating a small amount

of  $La^{3+}$  cations were substituted by  $Co^{+3}$  [26]. In addition, a zoom in 2 $\theta$  between 32° and 35° relating to the most intense diffraction peak of LaCoO<sub>3</sub> perovskite shows a splitting characteristic of rhombohedra symmetry. The addition of Sr resulted in the overlapping of both peaks and made an asymmetric wide peak of a distorted rhombohedra (JCPDS card 048-0122) because of the formation of a spinel-type structure [27]. Therefore, a gradual transformation in the characteristic pattern from the rhombohedral structure to the rhombohedral distorted structure happened as Sr content increased.



Fig. 1. XRD patterns of (a) Sr0.1Cuy and (b) SrxCu0.25 perovskite samples

sample	Surface composition (at%)					
	Sr <sub>seg</sub> /S <sub>tot</sub>	Sr/Co	Cu/Co	$Cu^{1+}/Cu^{2+}$	Co <sup>2+</sup> /Co <sup>3+</sup>	Oads/ Olatt
LaCoO <sub>3</sub>	-	0 (0) <sup>a</sup>	0 (0)	-	22.1	121.2
Sr0Cu0.25	-	0 (0)	0.38 (0.33)	11.2	18.2	181.5
Sr0.1Cu0.25	0.54	0.33 (0.26)	0.41 (0.33)	16.6	17.5	192.6
Sr0.2Cu0.25	0.63	0.61 (0.53)	0.45 (0.33)	21.2	17.1	198.3
Sr0.1Cu0	0.53	0.30 (0.2)	0 (0)	-	21.4	132.3
Sr0.1Cu0.50	0.61	0.51 (0.4)	1.27 (1)	34.5	15.1	226.1

Table 3. Surface atomic ratios of different compounds in the perovskites

<sup>a</sup> Nominal values are in parentheses.

#### 3.1.2. Textural and physical properties

The textural and physical properties of synthesized samples including BET surface area, pore volume and bulk elemental composition are given in **Table 3**. LaCO<sub>3</sub> had a specific surface area of  $9.8 \text{ m}^2/\text{gr}$  and a total pore volume of  $0.09 \text{ cm}^3/\text{gr}$ . It can be seen that the BET surface area and pore volume of the modified samples are close to LaCO<sub>3</sub> and no significant differences were observed after the incorporation of Cu and Sr. The lowest BET surface area and pore volume belonged to Sr0.2Cu0.5, due to the segregation of some CuO oxides which may block the access to the pores [11, 22].

The bulk elemental composition of the samples measured by XRF shows that the real values of the elements are close to theoretical ones. Actually, some little differences can be observed which may be attributed to experimental errors. Another possible explanation is due to formation of some intermediate valence state metal ions during the synthesis process which affects the XRF results [26]. It should be noted that theoretical values are only based on saturated metal ions.

The surface elemental compositions based on XPS are shown in Table 4. The ratio of segregated Sr to total Sr was chosen to investigate accommodation capacity of Sr in LaCoO<sub>3</sub> lattice. It can be clearly observed that ratio of Sr<sub>seg</sub>/S<sub>tot</sub> raised with increasing Sr and Cu doping degrees. For instance, the  $Sr_{seg}/S_{tot}$  of the samples increased from 0.54 to 0.63 m<sup>2</sup>/g and 0.53 to 0.61 cm<sup>3</sup>/g when x and y respectively increased from 0.1 to 0.2 and 0 to 0.5. These phenomena demonstrated that there was a limited capacity for Sr element to be incorporated into LaCoO<sub>3</sub> lattice. On the other hand, the real surface ratios of Sr/Co and Cu/Co were higher than the theoretical ones and the differences became more significant as Sr and Cu doping degrees increased. This further confirmed the difficulty of Sr and Cu ions incorporation into LaCoO<sub>3</sub> lattice [22].

The reduction reactivity of the synthesized samples was investigated by H<sub>2</sub>-TPR and acquired results are shown in **Fig. 2**. It should be first noted that La and Sr were not reducible in the range of temperatures studied here [28]. The reduction profiles were divided into two regions, called  $\alpha$ -reduction for temperatures below 500 °C and  $\beta$ reduction for temperatures above 500 °C. In general, the peaks in the  $\alpha$ -reduction region are due to the reduction of cation defective sites at oxygen vacancies while the those in the  $\beta$ -reduction region are derived from the reduction of metal species in the bulk of perovskite [17, 23].

In the case of  $LaCoO_3$ , there were four reduction peaks at temperatures about 370, 420, 585 and 635 °C. According to the literature [26, 27] the two first peaks at temperatures below 500 °C are due to the reduction of  $Co^{3+}$  ions to  $Co^{2+}$  while the last two are associated with the reduction of Co<sup>2+</sup> ions to metallic Co in the bulk of the LaCoO<sub>3</sub> structure. For La<sub>0.9</sub>Sr<sub>0.1</sub>Co<sub>1-y</sub>Cu<sub>y</sub>O<sub>3</sub> samples (Fig. 2a), a new reduction peak at temperature about 305  $^{\circ}$ C was detected as the reduction of Cu<sup>2+</sup> to Cu<sup>+</sup> [12, 17]. The peak at 360 °C arose from the overlapping reduction of  $Cu^+$  to metallic Cu and  $Co^{3+}$  to  $Co^2$  and the last peak at temperature 540 °C was associated with the reduction of  $Co^{2+}$  ions to metallic Co. it can be observed that the reduction temperatures shifted significantly to lower temperatures in comparison with LaCoO<sub>3</sub> which means the presence of Cu in the  $LaCoO_3$  structure eased the reducibility of the Co species. On the other hand, the peak area increased as the content of Cu in the LaCoO<sub>3</sub> structure enhanced, demonstrating the number of consumed hydrogen moles increased. The more hydrogen consumption, the higher number of reducible species.

The TPR curves for  $La_{1-x}Sr_xCo_{0.75}Cu_{0.25}O_3$  samples in **Fig. 2b** show similar trends to those of La0.9Sr0.1Co1. <sub>y</sub>Cu<sub>y</sub>O<sub>3</sub> samples with three reduction peaks at about 305, 360 and 540 °C. It can be observed that the enhancement of Sr substitution degree caused the movement of reduction peaks to lower temperatures. Furthermore, the area of the reduction peaks increased as the amount of Sr enhanced. These behaviors demonstrate that the

3.1.3. H<sub>2</sub>-TPR

lactorial configuration				
Run	Sr	Cu	Activation	
Number	substitution	substitution	Energy	
	degree (x)	degree (y)	(kj/mol)	
1	0.20	0.25	58.38	
2	0.10	0.25	54.02	
3	0.20	0.00	62.19	
4	0.20	0.50	64.19	
5	0.00	0.00	70.48	
6	0.10	0.00	60.34	
7	0.00	0.50	61.17	
8	0.00	0.25	58.85	
9	0.10	0.50	58.31	

Table 4. Design matrix and the activation energies for full



Fig. 2.  $H_2$ -TPR profiles of (a) Sr0.1Cuy and (b) SrxCu0.25 perovskite samples.

reduction ability of Co and Cu was facilitated in the presence of Sr ions. As we know, Sr is not reducible in the TPR temperature range, so generation of oxygen vacancies due to the positive charge defects after the substitution of  $La^{3+}$  by  $Sr^{2+}$  is the only mechanism available to improve the reducibility. In fact, an increase in the area of  $\alpha$ -reduction peaks to  $\beta$ -reduction peaks was observed which proves the mentioned mechanism.

#### 3.1.4. XPS investigations

XPS technique was applied to investigate the oxidation state of each element and acquired results for Cu, Sr, Co and O are given in **Figs. 3-6**, respectively.

For Cu 2p in Fig. 3, the peaks at 933 eV (Cu  $2p_{3/2}$ ) and 953 eV (Cu 2p<sub>1/2</sub>) and their satellite at 942 eV are characteristic of Cu<sup>2+</sup>. In addition, a little peak at 932.4 eV is detected which is the signal of Cu<sup>+1</sup>. The results demonstrates that Cu was mainly in the oxidation state of +2 and a small amount of +1 oxidation state coexisted [29]. The redox cycle  $Co^{2+} + Cu^{2+} \leftrightarrow Co^{3+} + Cu^{+}$ may be the main reason for the formation of  $Cu^{+2}$ . According to **Table 4**, the ratio of  $Cu^{1+}/Cu^{2+}$  increased when either the amount of Cu or Sr was enhanced. For Sr 3d in Fig. 4, Sr  $3d_{5/2}$  spectra were deconvoluted into two contributions located at 131.9 and 133.6 eV. The first peak at low binding energy is attributed to Sr in the perovskite lattice while the one at high binding energy is due to Sr surface species [30]. According to Table 4, addition of either Cu or Sr caused an increase of the  $Sr_{seg}/S_{tot}$  ratio.

The relevant spectra of Co 2p in Fig. 5 shows two main peaks at 779.7 eV (Co 2p3/2) and 794.9 eV (Co 2p1/2) as the signals of  $Co^{3+}$ , while the small peaks at 781.8 eV (Co 2p3/2) and 796.8 eV (Co 2p1/2) are due to  $Co^{2+}$  [22, 28]. For La<sub>0.9</sub>Sr<sub>0.1</sub>Co<sub>1-v</sub>Cu<sub>v</sub>O<sub>3</sub> samples, the acquired results in Table 4 show that the ratio of  $Co^{2+}/Co^{3+}$ decreased as the amount of Cu enhanced. The formation of  $Co^{2+}$  in these cases is probably related to the redox cycle  $Co^{2+} + Cu^{2+} \leftrightarrow Co^{3+} + Cu^+$  [21]. As  $Cu^{2+}$  ions are substituted at  $Co^{3+}$  sites, some  $Co^{2+}$  must be oxidized to Co<sup>3+</sup> to maintain electrical neutrality, so the ratio of  $Co^{2+}/Co^{3+}$  decreases [5]. For  $La_{1-x}Sr_xCo_{0.75}Cu_{0.25}O_3$ samples, the ratio of  $Co^{2+}/Co^{3+}$  slightly decreased as the amount of Sr enhanced. This behavior indicates that charge compensation in La<sub>1-x</sub>Sr<sub>x</sub>Co<sub>0.75</sub>Cu<sub>0.25</sub>O<sub>3</sub> samples seems to be slightly accomplished by the oxidation of Co<sup>2+</sup> to Co<sup>3+</sup> alongside the formation of oxygen vacancies.

From **Fig. 6**, two peaks at binding energies of 528.7 and 531.5 eV are observed which are attributed to lattice oxygen bonded to cations in the crystal structure ( $O_{latt}$ , e.g.  $O^{2-}$ ) and adsorbed oxygen species ( $O_{ads}$ , e.g.  $O_{2-}$ ), respectively. The adsorbed oxygen species are mainly associated with surface defects such as oxygen vacancies [17, 22]. As given in **Table 4**, the ratio of  $O_{ads}$  / $O_{latt}$  increased when the doping degree of either Cu or Sr enhanced, indicating the formation of oxygen after the deformation of perovskites. These results are in good agreement with those of H<sub>2</sub>-TPR, where the area of  $\alpha$ -reduction peaks to  $\beta$ -reduction peaks increased after the addition of either Sr or Cu into the LaCoO<sub>3</sub>



Fig. 3. Cu 2p XPS spectra of the perovskites.







Fig. 5. Co 2p XPS spectra of the perovskites.



Fig. 6. O 1s XPS spectra of the perovskites.

structure. Furthermore, the first peak attributed to the lattice oxygen species shifted to lower binding energies as the amount of either Cu or Sr enhanced, implying these oxygen species became more mobile. The formation oxygen defects after the incorporation of Cu and Sr adsorbs gaseous oxygen and creates chemisorbed oxygen species through catching electrons, leading to the movement and transformation of the adsorbed and lattice oxygen species [26]. These behaviors are in good accordance with the movement of reduction peaks to lower temperatures in the TPR results.

#### 3.2. Catalytic results and analysis of data

The catalytic activity of the elaborated perovskites in methane total combustion in the temperature range of 350-750 °C is given in **Fig. 7**. For comparison of catalytic activities, the activation energies were calculated using the Arrhenius equation. The design matrix obtained by the full factorial design and their corresponding activation energies are given in Table 5. Analysis of variance (ANOVA) was employed to evaluate the effects of the process variables (Cu and Sr) and their interactions on the activation energies (**Table 6**).

F-test and P-value were employed to examine the obtained model, standard residual/ error, and significance of each parameter. The F-test is defined as the ratio of the mean square (MS) to the residual mean square (MSresid). MS is the mean square of the factors or interactions while MSresid is the mean square of errors. The p-value is the probability of rejecting the null hypothesis of a study question, assuming that the null



Fig. 7. Methane conversion over the perovskites as a function of temperature.

Table 6. Analysis of variance for the activation energy from the experimental design

Source	Sum of squares	Degree of freedom	Mean Square	F-value	p-value
Model	166.65	5	33.33	38.52	0.0064
A-Cu	14.54	1	14.54	16.80	0.0263
B-Sr	5.49	1	5.49	6.35	0.0862
AB	31.98	1	31.98	36.96	0.0089
$A^2$	64.90	1	64.90	75.00	0.0032
$\mathbf{B}^2$	49.73	1	49.73	57.47	0.0048

hypothesis is correct. The smaller the p-value, the stronger evidence against the hypothesis. In statistical studies, a large F-test value with a p-value less than 0.05 indicates that a term is significant at 95% confidence limit [19, 31].

From ANOVA results, the F-test value of 38.52 and the p value of 0.0064 mean that the model is statistically significant and can estimate the activation energy with Cu and Sr doping degrees as the variables. Furthermore, factor A and interactions AB,  $A^2$  and  $B^2$  with p-values less than 0.05 are statistically significant.

A quadratic equation for the activation energy as the function of actual variables was obtained as follows:

Activation Energy 
$$(kJ / mol) = 69.78 - 63.11 \times Cu - 137.57 \times Sr$$
  
+113.10×Cu×Sr+91.14×Cu<sup>2</sup>+498.66×Sr<sup>2</sup>  
(3)

where Cu and Sr are substitution degrees. The correlation coefficient ( $R^2$ ) of **Eq. 3** is 0.959, representing a fitting with high accuracy for the model. Moreover, the linear distribution of the experimental

points along the idealized trend in **Fig. 8** indicates that the deviations of predicted values from experimental values are low.

### 3.2.1 Response surface (contour) plots and Interactions effects

Eq. 3 was employed to obtain a contour plot for the activation energy as a function of Cu and Sr doping degrees. The acquired results are shown in Fig. 9. The contour plot is a graphical representation of Eq. 3. As shown in Fig. 9, the activation energy decreases with the simultaneous increase of Cu and Sr doping degrees up to the range of 0.07-0.15 for Sr and 0.2-0.4 for Cu. In this range, the activation energy is about 54 kj/mol. It can be observed that at high levels of Cu and Sr doping degrees, the activation energy is high.

Two-factor interaction plot (**Fig. 10**) can also provide useful information about the interaction of Cu and Sr doping degrees (A  $\times$  B). According to **Fig. 10**, at the lowest Sr doping degree (Sr=0), the activation energy decreased from about 70 to 61 kj/mol when Cu doping



Fig. 8. Predicted vs. actual values for activation energy.



Fig. 9. Contour plot describing the response surface for activation energy as a function of Cu vs. Sr doping degrees.



**Fig. 10**. Interaction effect of  $A \times B$  on the activation energy.

degree increased from 0 to 0.5. However, the effect of Cu doping degree became weaker at superior Sr doping degree. For instance, the effect of Cu doping degree was negligible when factor B (Sr doping degree) was set at about 0.15. Further increasing of factor B from 0.15 caused an inverse effect on the activation energy so that the activation energy increased when Cu doping degree increased. On the other hand, at the high level of Cu doping degree, increasing Sr doping degree brings about a minimum value of the activation energy at Sr doping degree =0.08 while at the low level of Cu doping degree, increasing Sr doping degree led to a nearly continuous decrease of the activation energy. These behaviors demonstrate that there is a limited capacity for LaCoO<sub>3</sub> to accommodate Sr and Cu into the lattice aiming at improving the catalytic combustion activity.

The incorporation of Cu and Sr into the LaCoO<sub>3</sub> structure altered crystallinity, BET specific surface area, reducibility, oxygen mobility and oxygen vacancies. It was observed from XRD results that the incorporation of Cu and Sr decreased crystallinity and led to segregation of some oxide phases at high levels of Cu and Sr doping degrees. This segregation of oxide phases caused reduction in the BET specific surface area due to blockage of access to some pores. Therefore, the main reason for the deterioration of the activity at high levels of Cu and Sr doping degrees was due to the decrease in crystallinity and BET specific surface area.

Partial substitution of La<sup>+3</sup> by Sr<sup>+2</sup> and Co<sup>+3</sup> by Cu<sup>+2</sup> in LaCoO<sub>3</sub> structure resulted in the formation of positive charge defects. It is suggested that these defects are balanced by the formation of oxygen vacancies (adsorbed oxygen species), as evidenced by O1s XPS, where it is observed that the  $O_{ads}$  / $O_{latt}$  ratio increases at elevated doping degrees of either Cu or Sr. It is known that adsorbed oxygen species are more active compared to lattice oxygen species due to higher accessibility and mobility [32]. The existence of more oxygen vacancies accelerated the oxygen mobility and increased oxygen capacity, so the reducibility in  $\alpha$ -reduction region improved, as revealed by H2-TPR results. Higher oxygen mobility, oxygen capacity and reducibility facilitated oxygen accessibility to methane and accordingly resulted in higher activity.

Apart from oxygen vacancies, lattice oxygen species also play important roles in oxidation of methane. According to Mars-Van-Krevelen mechanism, after adsorption and dissociation of  $O_2$  molecules on the perovskite surface, they are incorporated into the crystal lattice of perovskite as  $O^2$  species and then are utilized in the oxidation reaction [33]. As indicated by H<sub>2</sub>-TPR results, addition of either Sr or Cu into the LaCoO<sub>3</sub> enhanced and eased reducibility in the  $\beta$ -reduction region. On the other hand, O1s XPS results showed that the mobility of lattice oxygen species improved after the incorporation of either Sr or Cu. The improved reducibility, oxygen capacity and oxygen mobility of lattice oxygen accelerate the movement of lattice oxygen from interior to surface and make them accessible to methane.

The difference in electronegativity of Cu (1.90) and Co (1.88) is another factor which could effect on metaloxygen binding interaction. The smaller difference in electronegativity between Cu and oxygen compared to Co and oxygen weakens the interaction of oxygen to Cu sites. This further proves our XPS results where it was observed that the oxygen mobility enhanced after incorporation of Cu into LaCoO<sub>3</sub> lattice. The weakened metal-oxygen binding interaction activates C-H bond of methane more easily, leading to higher activity [25].

Many reports on oxidation of methane over perovskite based catalysts can be found in literature and we have summarized some of the best reported results in **Table 7**. LaAl<sub>0.9</sub>Pd<sub>0.1</sub>O<sub>3</sub> by Yang et al. [34] stands out because of its lower T<sub>90</sub> (reaction temperature for 90% conversion of methane). Experiments in the present study have been obtained under most unfavorable reaction conditions, i.e. GHSV = 64000 h<sup>-1</sup> and CH<sub>4</sub> = 2 vol.% in the feed stream, resulting in higher T<sub>90</sub>. Despite more unfavorable reaction conditions as compared to the literature results in **Table 7**, comparable results have been achieved in this work.

#### 4. Conclusions

The catalytic performance of La<sub>1-x</sub>Sr<sub>x</sub>Co<sub>1-y</sub>Cu<sub>y</sub>O<sub>3</sub> perovskites was optimized by changing Sr and Cu doping degrees using full factorial deign of experiment. The substitution of  $Sr^{+2}$  at  $La^{+3}$  sites and  $Cu^{+2}$  at  $Co^{+3}$ sites led to the formation of charge imbalances which was subsequently compensated by the creation of oxygen vacancies. Although these substitutions decreased the crystallinity, the catalytic activity enhanced in combustion of methane. Formation of oxygen vacancies increased oxygen capacity, oxygen mobility and reducibility which accordingly enhanced exchange capacity between lattice oxygen and gas phase oxygen. A minimum in the activation energy was observed by increase of Sr and Cu doping degrees at moderate values of the corresponding parameters. The best performance belonged to Sr0.1Cu0.25 with activation energy of 54.02 kj/mol. The segregation of oxide phases and decrease of BET specific surface area were the main reasons for the deterioration of activity at high levels of Sr and Cu doping degrees.

**Table 7.** Summarized perovskite-based catalysts for methane combustion

catalyst	Feedstream	GHSV,	T <sub>90</sub>	Ref.
	(vol%)	$h^{-1}$		
La <sub>0.6</sub> Sr <sub>0.4</sub> MnO	0.25%	5625	480	[33]
	CH <sub>4</sub> , 1%			
	Ne,			
	balance O <sub>2</sub>			
$LaCo_{0.8}Fe_{0.2}O_3$	0.25%	5625	490	[4]
	CH <sub>4</sub> , 1%			
	Ne,			
	balance O <sub>2</sub>			
$La_{0.75}Ag_{0.25}FeO_{2}$	1% CH4	5800	475	[23]
Eu0.757 160.251 003	balance air	5000	175	[23]
			100	50 F3
$BaCe_{0.6}Mn_{0.4}O_3$	1% CH <sub>4</sub> ,	20L·g⁻	423	[35]
	balance air	<sup>1</sup> •h <sup>-1</sup>		
LaAl <sub>0.9</sub> Pd <sub>0.1</sub> O <sub>3</sub>	1% CH4,	15L·g⁻	400	[34]
	20% O <sub>2</sub> ,	$1 \cdot h^{-1}$		
	balance N <sub>2</sub>			
$La_{0.9}Sr_{0.1}Co_{0.75}Ci_{10.25}O_{3}$	2% CH4	64000	550	This
Lu0.9510.1000.75Cu0.25C5	18% O2	01000	220	work
	balance $N_2$			

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